



File Geometry Reporting SESAM interface Help

Input point coordinates [mm] **Add point (coords)**  
 Copy point (relative)  
 Move point (relative)

Point x (horizontal) [mm]: 0.0  
 Point y (vertical) [mm]: 0.0

Input line from "point number" to "point number"  
 From point number: 0 **Add line**  
 To point number: 0

Delete lines and points (or left/right click and use "Delete key")  
 Line number (left click): 7 **Delete line** **Delete prop.**  
 Point number (right click): 0 **Delete point**

Structural and calculation properties input below:

span	s	pl.thk	web_h	web_thk	fl_w	fl_thk
3.6	750.0	18.0	400.0	12.0	250.0	12.0
[m]	[mm]	[mm]	[mm]	[mm]	[mm]	[mm]
kpp	kps	km1	km2	k3		
1.0	1.0	12.0	24.0	12.0		
[kps]	[kps]	[km1]	[km2]	[k3]		
sig_y1	sig_y2	sig_x	tau_y1	stf type		
100.0	100.0	101.5	5.0	T		
[MPa]	[MPa]	[MPa]	[MPa]	[type]		

Material yield [MPa]: 355.0  
 Pressure side (p-plate, s-stf): p

Select structure type:  
 BOTTOM (Internal, pressure from comp.)  
 Show structure types  
☒ z\* optimization **Add structure to line**

**Find compartments** **External pressures**

Comp. no.: 2  
 Tank content:  **Display current compartments**  
 Tank density: 0 [kg/m³]  
 Overpressure: 25000 [Pa] **Set compartment properties.**  
 Max elevation: 0.0  
 Min elevation: 0.0  
 Acceleration [m/s²]:  **Delete all tanks**

Check to see available shortcuts

CTRL-Z Undo geometry action  
 CTRL-C Copy selected point  
 CTRL-M Move selected point  
 CTRL-Q New line (right click two points)  
 CTRL-S Assign structure properties to clicked line  
 CTRL-DELETE Delete structure properties from clicked line  
 DELETE Delete active line and/or point  
 CTRL-E Copy line properties from active line  
 CTRL-D Paste line properties to active line  
 Mouse click left/right - select line/point  
 Arrows left/right - previous/next line

Static and dynamic accelerations **line7**  
 Static acceleration [m/s²]: 9.81  
 Dyn. acc. loaded [m/s²]: 3.0 **Set accelerations**  
 Dyn. acc. ballast [m/s²]: 3.0

Optimize selected line/structure (right click line):  
**OPTIMIZE** **MultiOpt** **SPAN**

Combination for line (select line). Change with slider:  
 OS-C101 Table 1 1: DNV a) 2: DNV b) 3: TankTest

Name	Stat. LF	Dyn. LF	Include?
ballast_bottom	0.0	0.7	<input checked="" type="checkbox"/>
loaded_static	1.3	0.0	<input checked="" type="checkbox"/>
ballast_static	1.3	0.0	<input checked="" type="checkbox"/>
loaded_bottom	0.0	0.7	<input checked="" type="checkbox"/>
Compartment4	1.2	0.7	<input checked="" type="checkbox"/>
Manual (pressure/LF)	0.0	1.0	<input checked="" type="checkbox"/>

Pressures for this line:  
 (DNV a/b loaded/ballast), tank test, manual)  
 Note that ch. 4.3.7 and 4.3.8 is accounted for.  
 DNV a [Pa]: {465279, 233597} DNV b [Pa]: {439799, 220435}  
 TT [Pa]: {335707} Manual [Pa]: {0,0}

**Load factors** **Load info**

Plate field span: 3.6 meters  
 Stiffener spacing: 750.0 mm  
 Plate thickness: 18.0 mm  
 Stiffener web height: 400.0 mm  
 Stiffener web thickness: 12.0 mm  
 Stiffener flange width: 250.0 mm  
 Stiffener flange thickness: 12.0 mm  
 Material yield: 355.0 MPa  
 Structure type/stiffener type: BOTTOM/7  
 Dynamic load variable: > horizontal  
 Plate fixation parameter:kpp: 1.0  
 Global stress: sig\_y1/sig\_y2: 100.0/100.0 MPa  
 Global stress: sig\_x: 101.5 MPa  
 Global shear: tau\_y1: 5.0 MPa  
 km1, km2, km3: 12.0/24.0/12.0  
 Pressure side (p-plate/s-stf): p

**SELECTED: line7**

Applied compartments: Compartment 4

Applied static/dynamic loads:  
 ballast\_bottom  
 loaded\_static  
 ballast\_static  
 loaded\_bottom

Section modulus: Wey1: 4.8300E+06 [mm³], Wey2: 1.7500E+06 [mm³]  
 Minimum section modulus: 1.7163E+06 [mm³]  
 Shear area: 5.1600E+03 [mm²]  
 Minimum shear area: 3.5296E+03 [mm²]  
 Plate thickness: 18.0 [mm]  
 Minimum plate thickness: 15.1 [mm]  
 Buckling results DNV-RP-C201:  
 Eq 7.19: 0.86 [eq 7.50: 0.92 [eq 7.51: -0.19 [7.52: 0.6]eq 7.53: 0.92 [z\*: 0.12  
 Fatigue results (DNVGL-RP-C203):  
 Total damage: NO RESULTS

# Documentation

2021  
Version 2.X

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## Theory

All calculations are according to the following DNVGL standards and recommended practices:

- DNVGL-OS-C101 Design of offshore steel structures, general - LRFD method
  - <http://rules.dnvgl.com/docs/pdf/DNVGL/OS/2018-07/DNVGL-OS-C101.pdf>
- DNV-RP-C203 Fatigue design of offshore steel structures
- DNV-RP-C201 BUCKLING STRENGTH OF PLATED STRUCTURES
  - <https://rules.dnvgl.com/docs/pdf/DNV/codes/docs/2010-10/RP-C201.pdf>

The logo for DNV-GL, consisting of the letters "DNV-GL" in a bold, dark blue, sans-serif font.

## Modelling

Modelling is done in upper left corner.

Right click: select point

You can copy or move the selected point by shortcut or clicking Buttons.

Left click: select line

A line is made by right clicking two points (or input point number)

<b>Input point coordinates [mm]</b>		<b>Add point (coords)</b>
Point x (horizontal) [mm]:	<input type="text" value="0.0"/>	<b>Copy point (relative)</b>
Point y (vertical) [mm]:	<input type="text" value="0.0"/>	<b>Move point (relative)</b>
<b>Input line from "point number" to "point number"</b>		
From point number:	<input type="text" value="0"/>	<b>Add line</b>
To point number:	<input type="text" value="0"/>	
<b>Delete lines and points (or left/right click and use "Delete key")</b>		
Line number (left click):	<input type="text" value="43"/>	<b>Delete line</b>
Point number (right click):	<input type="text" value="0"/>	<b>Delete point</b>

Speed up your modelling **significantly** by using the shortcuts:

CTRL-Z	Undo modelling
CTRL-P	Copy a selected point
CTRL-M	Move a selected point
CTRL-Q	New line between two selected points
CTRL-S	Assign properties to a selected line
CTRL-DELETE	Delete the structural properties from the selected line

- DELETE** Delete selected line/point
- CTRL-E** Select a line and copy the properties of this line
- CTRL-D** Paste structural properties to a selected line

Left and right arrow to change current line.

## Assigning properties

Input properties manually or click the button indicated below to set the values.

Values are set by clicking “Add structure to line”. This also applies to fatigue properties. If you have added a property to a line and want to use the same for the next line, just press “Add structure to line” on the new line.

All beam sections are recorded. If you want to apply an existing, choose it from the drop down menu. Then press “Save and return structure”.

The screenshot shows the 'Define structure properties' window. Red callout boxes highlight the following features:

- Define plate and stiffener properties.** Points to the 'Add line' button and the 'Delete lines and points' section.
- Define buckling calculation properties.** Points to the 'Find compartments' button.
- Define fatigue properties.** Points to the 'FLS' (Fatigue Limit State) button.

The main window displays the following information:

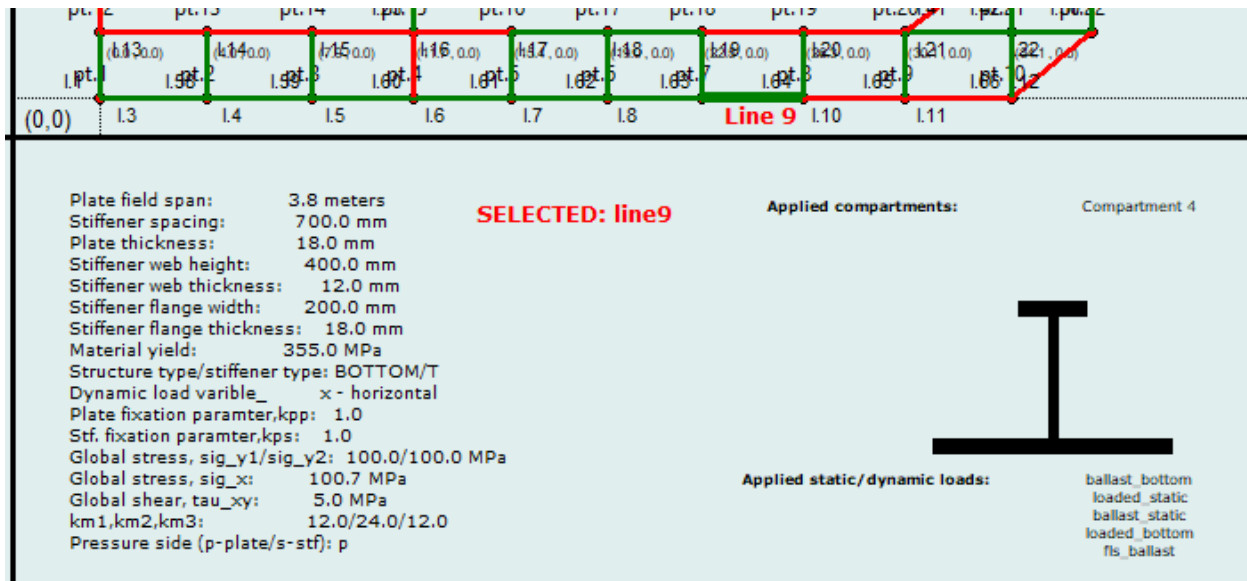
- Input line from "point number" to "point number"**: From point number: 0, To point number: 4.
- Structural and calculation properties input below:**
  - span: 700.0 [mm]
  - pl\_thk: 18.0 [mm]
  - web\_thk: 12.0 [mm]
  - fl\_thk: 14.0 [mm]
  - kpp: 1.0
  - kps: 1.0
  - km1: 12.0
  - km2: 24.0
  - k3: 12.0
  - sig\_y1: 100.0
  - sig\_y2: 100.0
  - sig\_x: 100.0
  - tau\_y1: 5.0
  - stf type: T
  - pressure side: p
  - Material yield [MPa]: 355.0
  - Select structure type -> BOTTOM
  - Internal, pressure from comp.
  - Add structure to line
- Define structure properties here --**
  - type: T
  - Plate thk: 18.0 [mm]
  - Web height: 400.0 [mm]
  - Web thk: 12.0 [mm]
  - Flange width: 250.0 [mm]
  - Flange thk: 14.0 [mm]
  - Existing sections: (dropdown menu)
  - Plate: 700.0x18.0
  - Web: 400.0x12.0
  - Flange: 250.0x14.0
- Diagram:** A cross-section diagram of a T-beam with dimensions b1, h, tw, tf, b, and z.
- 3D Model:** A 3D model of a girder with labels for PLATE, STIFFENER, GIRDER, and GIRDER length (Lg).
- Buttons:** Show structure types, Find compartments, Save and return structure.

By default  $z^*$  is ticked. This affects the buckling results and will generally give lower utilization than using  $z^* = 0$ . See description below.

$z^*$  is the distance from the neutral axis of the effective section to the working point of the axial force.  $z^*$  may be varied in order to optimise the resistance.  $z^*$  should then be selected so the maximum utilisation found from the equations (7.50) to (7.53) or (7.54) to (7.57) is at its minimum, see also Commentary Chapter 10. The value of  $z^*$  is taken positive towards the plate. The simplification  $z^* = 0$  is always allowed.

## Display properties

If you click a line properties is displayed in the window below as seen next.



## Define tanks

Tanks are searched for when clicking “Find compartments”. Non watertight structure are ignored. For information on structure types click “Show structure types”.

By default tank content density is set to 0.

After tanks are found content and overpressure must be defined as seen next.

Find compartments

External pressures

Comp. no.: **2**

2  
3  
4  
5

Tank content : fresh water

Tank density : 1000 [kg/m<sup>3</sup>]

Overpressure : 25000.0 [Pa]

Max elevation : 30.9

Min elevation : 2.5

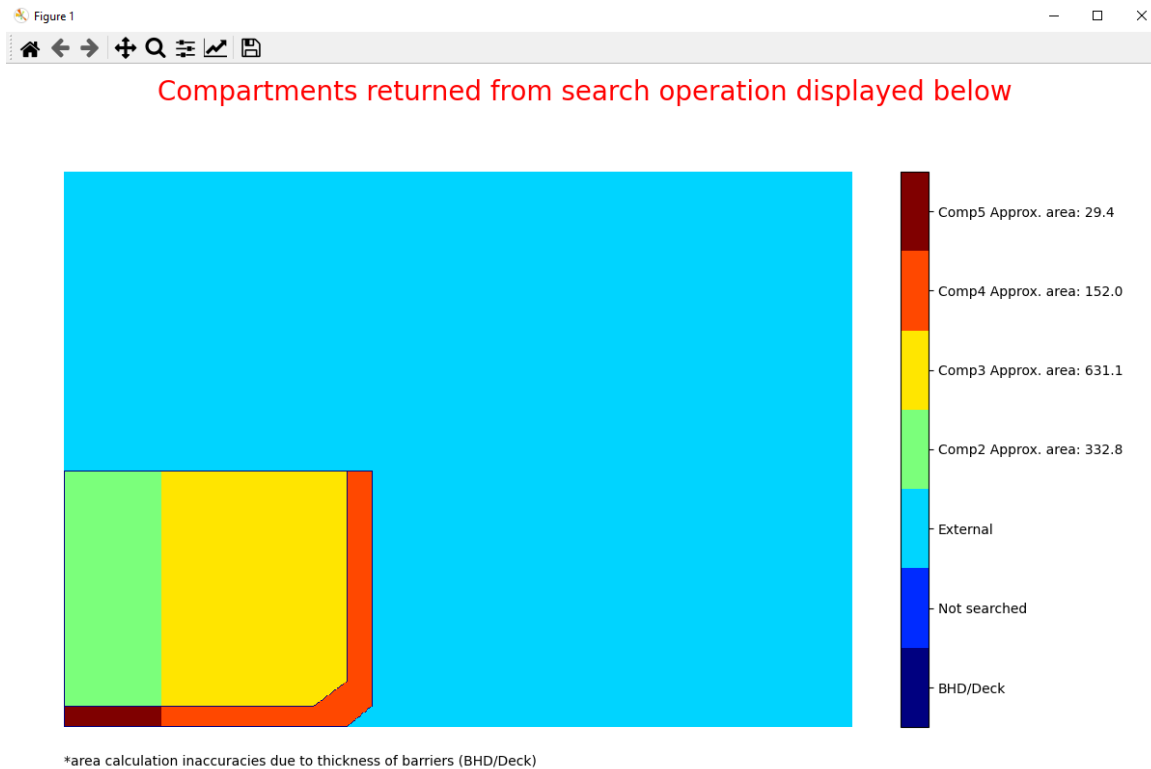
Display current compartments

Set compartment properties.

Delete all tanks

Accelerations [m/s<sup>2</sup>]:  
static: 9.81 , dynamic loaded: 3.0 , dynamic ballast: 3.0

If you press “Display current compartments” after doing a compartment search, the result of the search is illustrated as seen next. Approximate area of the respective compartments is also shown.



## Setting accelerations

Accelerations applies to tank content. I is set in the upper right corner as seen next.

— □ ×

**Static and dynamic accelerations** line10

Static acceleration [m/s <sup>2</sup> ]:	<input type="text" value="9.81"/>	<input type="button" value="Set accelerations"/>
Dyn. acc. loaded [m/s <sup>2</sup> ]:	<input type="text" value="3.0"/>	
Dyn. acc. ballast [m/s <sup>2</sup> ]:	<input type="text" value="3.0"/>	



## Define external pressures

Click “External pressures” to define pressures acting on the structures.

**NOTE:**

**FOR DYNAMIC EQUATION THE FOLLOWING APPLIES**

**X (horizontal) used for BOTTOM, BBT, HOPPER, MD**

**Z (vertical) used for BBS, SIDE\_SHELL, SSS**

**After new window is opened:**

- 1. Make dynamic loads**
  - a. Dynamic loads are made by defining up to 3rd degree equations. X or Y direction depends on the defined structure type.**
  - b. Note that you can define a constant dynamic load by using Constant (Constant (C)) only.**
- 2. Static loads are calculated according to depth.**
- 3. To apply a defined load to a line or multiple lines:**
  - a. a. Select load by clicking the created load**
- 4. Click the lines that shall have the load. Click the button “Press to add selected lines to selected load”**
- 5. When finished press the button in the upper right corner.**

Load properties

### 1. Dynamic loads

Define dynamic loads as an polynomial curve.  
Can be third degree, second degree, linear or constant

Input load name:

Third degree poly [x^3]:

Second degree poly [x^2]:

First degree poly [x]:

Constant [C]:

Load condition:

Limit state:

**Create dynamic load**

### 2. Static loads

Hydrostatic loads defined by draft.

Define name of static load:

Define static draft from sea:

Select load condition:

**Create static load**

### 3. Slamming pressure

Load name:

Pressure [Pa]:

**Create slamming load**

Press this to: Save loads and close the load window.

Press to add selected lines to select load

Select a load in "3." to and then choose lines to apply to load (select by clicking lines). Alternatively define manually ----->

Mouse left click: select lines to loads  
Mouse right click: clear all selection  
Shift key press: add selected line  
Control key press: remove selected line

Properties selected load is:

Name of load: ballast\_side  
Polynomial (x^3): 0.0  
Polynomial (x^2): 303.0  
Polynomial (x): -3750.0  
Constant (C): 153000.0  
Load condition: ballast  
Limit state: ULS  
Is external? True  
Static draft: None

## Load combinations

Load combinations are created automatically after external pressures are defined.  
Some comments on the loads.

1. According to DNVGL-OS-C101
2. Highest pressure are chosen w.r.t. tank filling.
3. You can deselect a load by manually inputting load factor to 0 or deselect include.

Combination for line (select line). Change with slider.:

OS-C101 Table 1 1: DNV a) 2: DNV b) 3: TankTest

1

Name:	Stat LF	Dyn LF	Include?
ballast_bottom	0.0	0.7	<input checked="" type="checkbox"/>
loaded_static	1.3	0.0	<input checked="" type="checkbox"/>
ballast_static	1.3	0.0	<input checked="" type="checkbox"/>
loaded_bottom	0.0	0.7	<input checked="" type="checkbox"/>
Compartment4	1.2	0.7	<input checked="" type="checkbox"/>
Manual (pressure/LF)	0.0	1.0	<input checked="" type="checkbox"/>

Pressures for this line:  
(DNV a/b [loaded/ballast], tank test, manual)  
Note that ch. 4.3.7 and 4.3.8 is accounted for.

DNV a [Pa]: [462698, 248632]      DNV b [Pa]: [546435, 248430]  
TT [Pa]: [335707]      Manual [Pa]: [0.0]

## Changing load factors

You can change default load factors and existing load factors using the button seen in the next illustration.

Load factors are based on standard DNV LRFD factors, but any values can be used.

OS-C101 Table 1 1: DNV a) 2: DNV b) 3: TankTest

1

Line:	Stat LF	Dyn LF	Include?
static_22m	1.3	0	<input checked="" type="checkbox"/>
static_15m	1.3	0	<input checked="" type="checkbox"/>
static_8m_tt	0	0	<input type="checkbox"/>
loaded_bottom	0	0.7	<input checked="" type="checkbox"/>
ballast_bottom	0	0.7	<input checked="" type="checkbox"/>
Compartment2	1.2	0.7	<input checked="" type="checkbox"/>
Manual (pressure/LF)	0	1	<input checked="" type="checkbox"/>

Pressures for this line:  
 DNV a/b [loaded/ballast], tank test, manual)  
 Note that ch. 4.3.7 and 4.3.8 is accounted for.

DNV a [Pa]: [329265, 229422] DNV b [Pa]: [298631, 212755]  
 TT [Pa]: [266326] Manual [Pa]: [0, 0]

**Load factors** Load info

Load factor modifications here.

### Static and dynamic load factors is specified here

Note that DNV is used as reference, but the load factors can be any other rule set such as ISO.

Condition a) - Static load factor "unknown loads"	1.3
Condition a) - Static load factor well defined loads	1.2
Condition a) - Dynamic load factor	0.7
Condition b) - Static load factor "unknown loads"	1
Condition b) - Static load factor well defined loads	1
Condition b) - Dynamic load factor	1.3
Tank test) - Static load factor "unknown loads"	1
Tank test) - Static load factor well defined loads	1
Tank test) - Dynamic load factor	0

**Return specified load factors and change existing**

**Table 1 Load factors  $\gamma_f$  for ULS**

Combination of design loads	Load categories			
	G	Q	E	D
a)	1.3	1.3	0.7	1.0
b)	1.0	1.0	1.3	1.0

Load categories are:  
 G = permanent load  
 Q = variable functional load  
 E = environmental load  
 D = deformation load  
 For description of load categories see Sec.2.

**4.4.2** When permanent loads (G) and variable functional loads (Q) are well defined, e.g. hydrostatic pressure, a load factor of 1.2 may be used in combination a) for these load categories.

**4.4.3** If a load factor  $\gamma_f = 1.0$  on G and Q loads in combination a) results in higher design load effect, the load factor of 1.0 shall be used.

**4.4.4** Based on a safety assessment considering the risk for both human life and the environment, the load factor  $\gamma_f$  for environmental loads may be reduced to 1.15 in combination b) if the structure is unmanned during extreme environmental conditions.

## Reviewing loads

Load calculations and results can be reviewed by clicking the "Load info" button. An example is seen in the next illustration.



Load info for line9



Loads for condition: loaded - dnva  
 static with acceleration: 9.81 is:  
 $1 \cdot 1.3 \cdot 221215.5 = 287580.2$   
 dynamic with acceleration: 3.0 is:  
 $1 \cdot 0.7 \cdot 198687.0 = 139080.9$

RESULT:  $287580.2 + 139081 = 426661.1$

-----  
 Loads for condition: ballast - dnva  
 dynamic with acceleration: 3.0 is:  
 $1 \cdot 0.7 \cdot 62231.0 = 43561.7$   
 static with acceleration: 9.81 is:  
 $1 \cdot 1.3 \cdot 150828.8 = 196077.4$

comp4 - static:  $1 \cdot 1.2 \cdot 310707.225000000003 + 25000.0 \cdot 1.3 = 405348.670000000004$   
 comp4 - dynamic:  $1 \cdot 0.7 \cdot 95017.500000000001 + 25000.0 \cdot 0 = 66512.25$

RESULT:  $43561.7 + 196077 = 239639.0$

-----  
 Loads for condition: loaded - dnvb  
 static with acceleration: 9.81 is:  
 $1 \cdot 1.0 \cdot 221215.5 = 221215.5$   
 dynamic with acceleration: 3.0 is:  
 $1 \cdot 1.3 \cdot 198687.0 = 258293.2$

RESULT:  $221215.5 + 258293 = 479508.7$

-----  
 Loads for condition: ballast - dnvb  
 dynamic with acceleration: 3.0 is:  
 $1 \cdot 1.3 \cdot 62231.0 = 80900.2$   
 static with acceleration: 9.81 is:  
 $1 \cdot 1.0 \cdot 150828.8 = 150828.8$

comp4 - static:  $1 \cdot 1.0 \cdot 310707.225000000003 + 25000.0 \cdot 1.3 = 343207.225000000003$   
 comp4 - dynamic:  $1 \cdot 1.3 \cdot 95017.500000000001 + 25000.0 \cdot 0 = 123522.750000000003$

RESULT:  $80900.2 + 150829 = 231729.0$

-----  
 Tank test for: comp4  
 $1 \cdot 1.0 \cdot 310707.2 + 25000.0 \cdot 1 = 335707$   
 Tank test for: comp4  
 $1 \cdot 1.0 \cdot 310707.2 + 25000.0 \cdot 1 = 335707$   
 Manual pressure:  
 $0.0 \cdot 1.0 \cdot 1 = 0.0$

OK

## Results

When clicking a line, results as presented in the window below. If the result for the clicked line is OK, the color of the line and text is green. If the result is NOT OK, the color of the line and text is red. Two examples are seen next.

All results ok

```
Section modulus: Wey1: 4.8300E+06 [mm^3], Wey2: 1.7500E+06 [mm^3]
Minimum section modulus: 1.7163E+06 [mm^3]

Shear area: 5.1600E+03 [mm^2]
Minimum shear area: 3.5296E+03 [mm^2]

Plate thickness: 18.0 [mm]
Minimum plate thickness: 15.1 [mm]

Buckling results DNV-RP-C201 (z* optimized):
|eq 7.19: 0.88 |eq 7.50: 0.92 |eq 7.51: -0.19 |7.52: 0.6|eq 7.53: 0.92 |z*: 0.12

Fatigue results (DNVGL-RP-C203):
Total damage: NO RESULTS
```

Section modulus not ok

Buckling not ok

```
Section modulus: Wey1: 4.2400E+06 [mm^3], Wey2: 1.4700E+06 [mm^3]
Minimum section modulus: 2.0739E+06 [mm^3]

Shear area: 4.6560E+03 [mm^2]
Minimum shear area: 4.1297E+03 [mm^2]

Plate thickness: 18.0 [mm]
Minimum plate thickness: 15.8 [mm]

Buckling results DNV-RP-C201 (z* optimized):
|eq 7.19: 0.9 |eq 7.50: 1.39 |eq 7.51: 0.35 |7.52: 0.81|eq 7.53: 0.73 |z*: 0.13

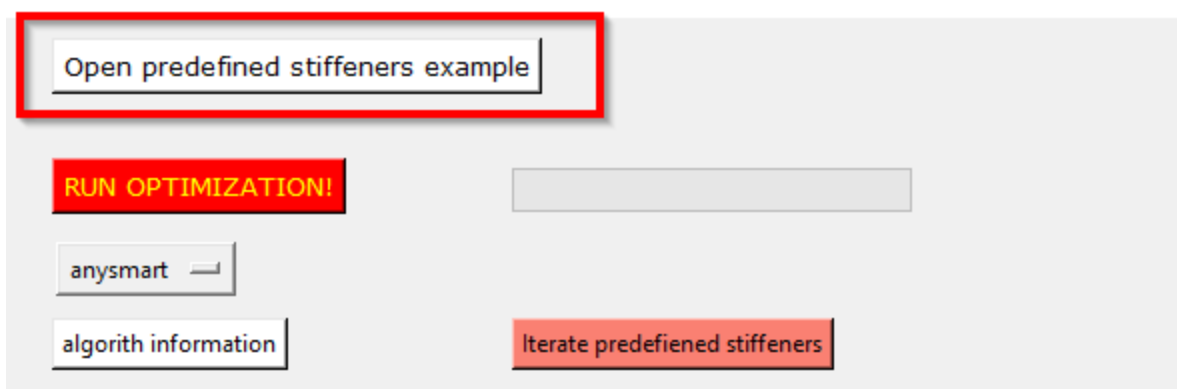
Fatigue results (DNVGL-RP-C203):
Total damage (DFF not included): 0.058 | With DFF = 2.0 --> Damage: 0.117
```

## Optimization

### Optimization iteration by predefined stiffeners

From 0.5 you can iterate by a defined set of stiffeners. Press the button marked below. Open a csv (or json) file. Then start your iterations. The only other input is the stiffener spacing and plate thickness.

To see how the input format is click the “open predefined stiffeners example” button. See illustrations next.



Note that the weight of your initial structure is ignored even though it is calculated. If the initial structure is in your predefined set it will be included in the evaluations.

Press the button indicated below to activate. A open file window will open when running the optimization.

**-- Structural optimizer --** Return and replace initial structure with optimized

Iterate predefined stiffeners

	Spacing [mm]	Plate thk. [mm]	Web height [mm]	Web thk. [mm]	Flange width [mm]	Flange thk. [mm]
Upper bounds [mm]	<input type="text" value="850.0"/>	<input type="text" value="25.0"/>	<input type="text" value="600.0"/>	<input type="text" value="35.0"/>	<input type="text" value="300.0"/>	<input type="text" value="40.0"/>
Iteration delta [mm]	<input type="text" value="50.0"/>	<input type="text" value="2.0"/>	<input type="text" value="50.0"/>	<input type="text" value="2.0"/>	<input type="text" value="50.0"/>	<input type="text" value="2.0"/>
Lower bounds [mm]	<input type="text" value="650.0"/>	<input type="text" value="10.0"/>	<input type="text" value="400.0"/>	<input type="text" value="15.0"/>	<input type="text" value="100.0"/>	<input type="text" value="20.0"/>

Estimated running time for algorithm: **7** seconds

RUN OPTIMIZATION!

## Single optimization

Single optimization is done by clicking a line and clicking the “OPTIMIZE” button.

1. Set the upper and lower bounds of the optimization.
2. Set the delta to be used for the searched. This is the step size of the optimization when using brute force method (for example anysmart).
3. Run the optimization.
4. If you are happy, return the properties by clicking the top button

Various checks in the optimization module:

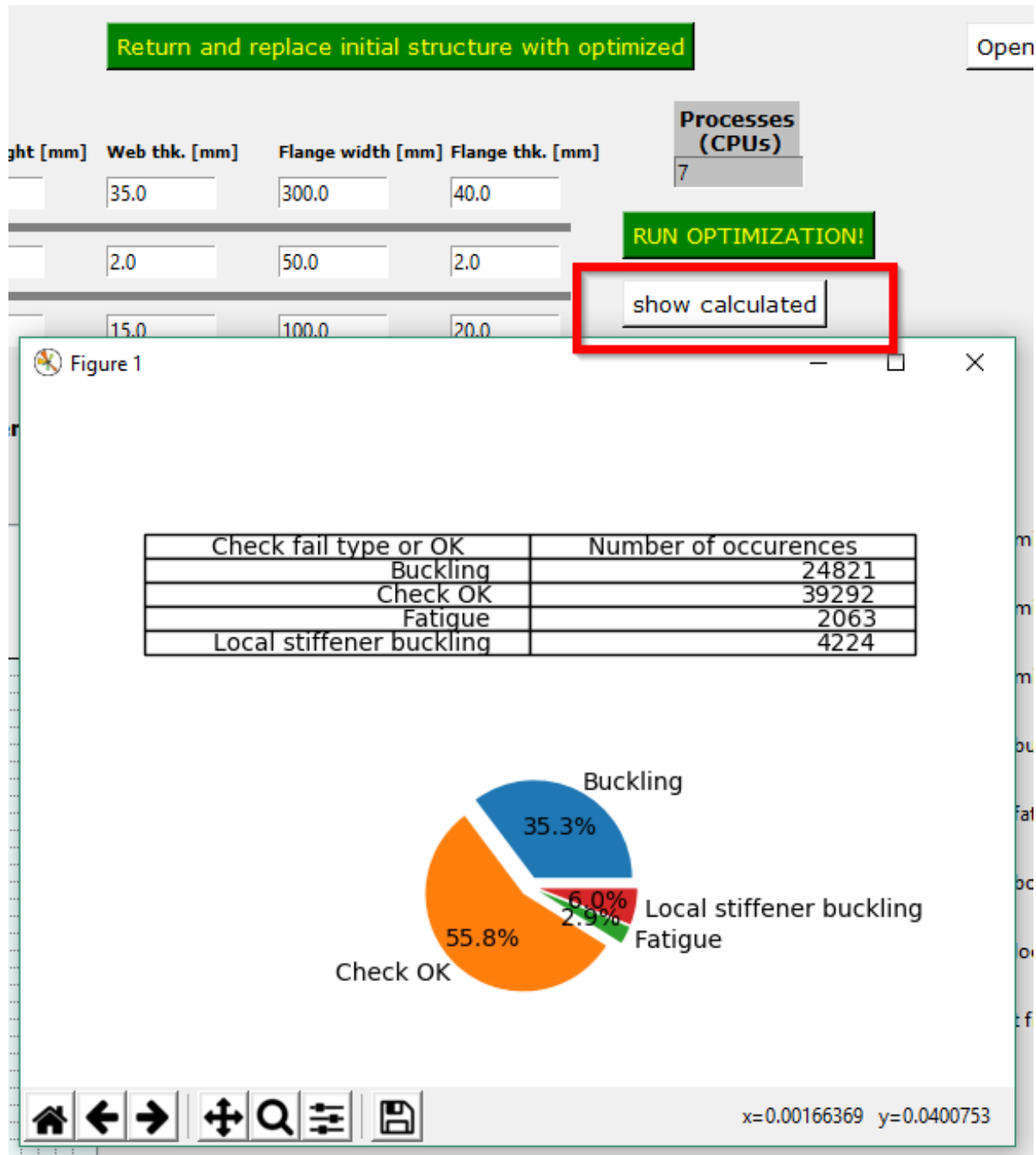
You can select the checks to be performed.

The weight filter ensures that only sections with a lower weight than the current minimum weight. This significantly speed up the calculations, but if you want to see the full distribution of the various checks this must be unchecked.

Check for minimum section modulus	<input checked="" type="checkbox"/>
Check for minimum plate thk.	<input checked="" type="checkbox"/>
Check for minimum shear area	<input checked="" type="checkbox"/>
Check for buckling (RP-C201)	<input checked="" type="checkbox"/>
Check for fatigue (RP-C203)	<input checked="" type="checkbox"/>
Check for bow slamming	<input type="checkbox"/>
Check for local stf. buckling	<input checked="" type="checkbox"/>
Use weight filter (for speed)	<input checked="" type="checkbox"/>

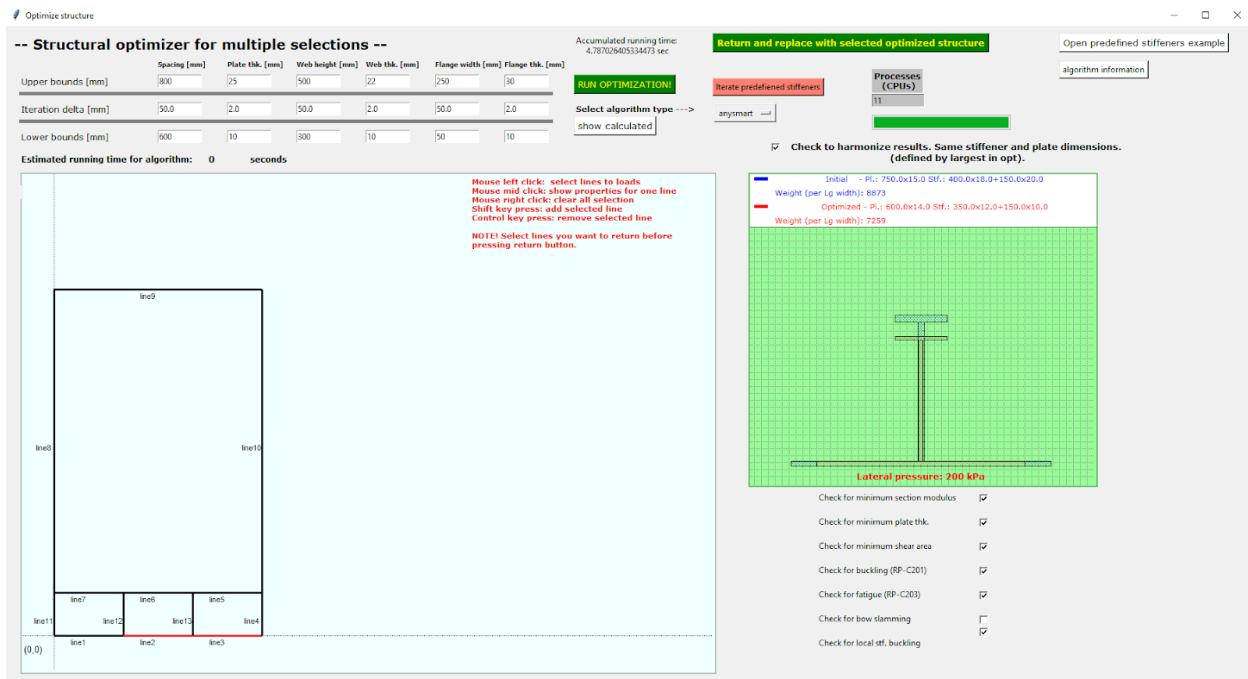
**If you press the “show calculated” button, you will get an overview of how many is ok and how many failed (and what criteria first failed). One “occurrence” is a one checked plate/stiffener combination.**





You will also be asked to save to a csv file. If you do not cancel, a csv file will ALL results will pre saved to your chosen location. If you open the file in excel you should see something like show next

## Multiple optimization



Multiple optimization is done by clicking the “MultiOpt” button.

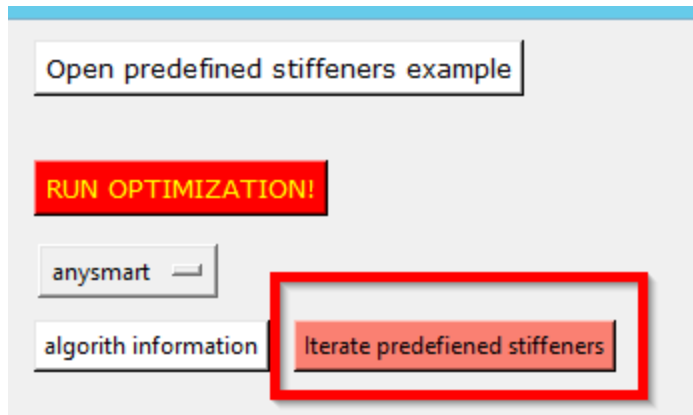
1. Same input on upper bounds, lower bounds and delta.
2. Click all the lines you want to include in the optimization.
3. Run the optimization.
4. Check the properties by **middle clicking** the line you ran.
5. If you are happy return the properties by clicking the top button. Remember to select the lines you want to return. Lines that have been optimized is marked orange.

The optimization can be **harmonized**. That means that the largest dimension found in the multiple optimization is used for all selected. This is done after all plates/stiffeners are checked. Harmonization can only be done in the multiopt option

Other options that can be set is explained in the single optimization chapter.  
When showing calculated you must have selected a line (middle click).

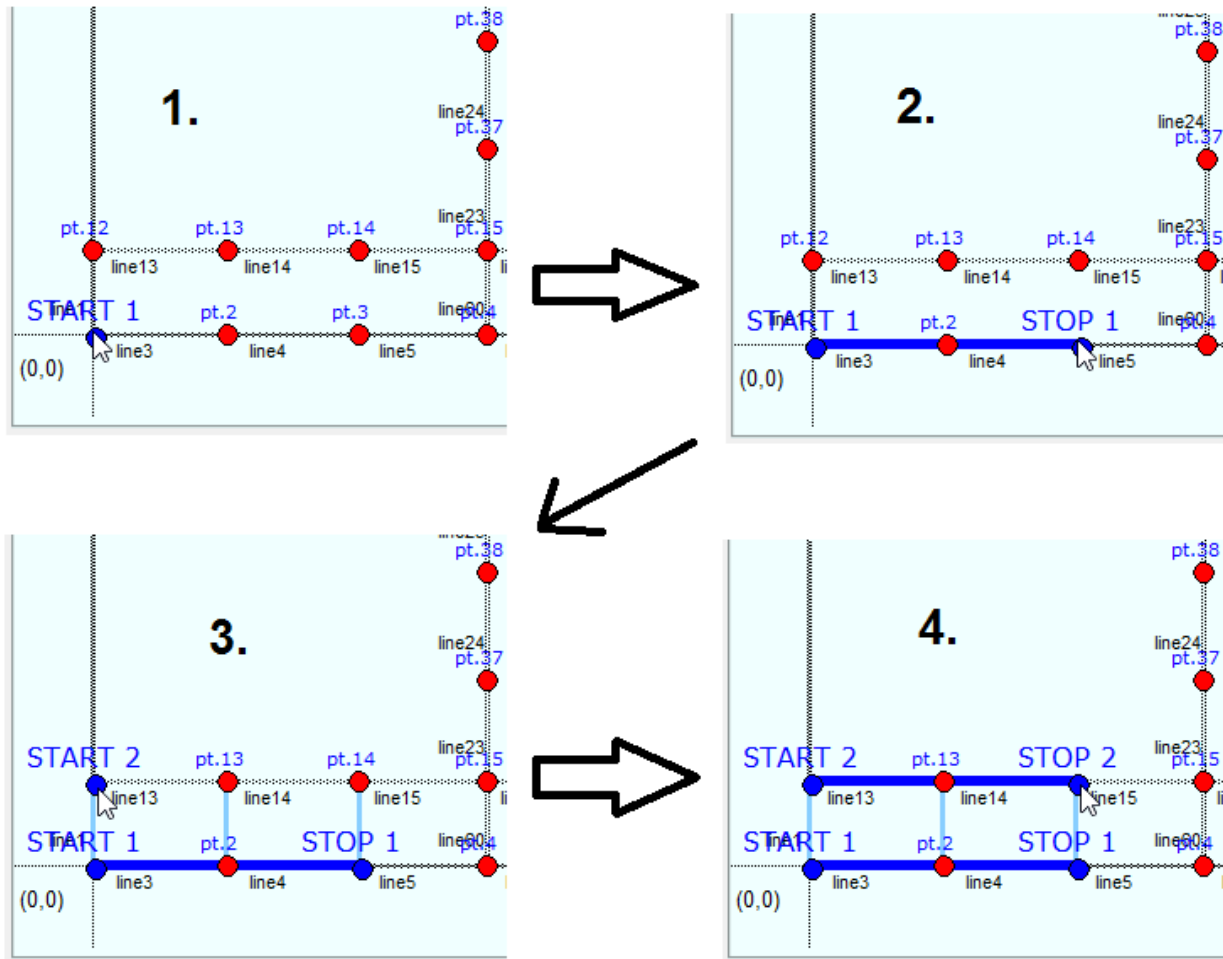
## Span optimization

**NOTE:** The span optimization is computationally heavy. It is recommended to use a set of predefined stiffeners.



The optimization is started as follows.

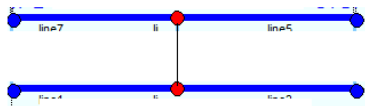
1. Start by clicking as illustrated next:



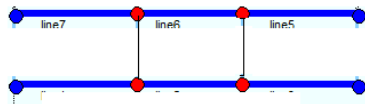
## 2. Then run optimization.

The program will calculate variations of even spans in your structure as illustrated next. This is an example and number of plate fields may vary.

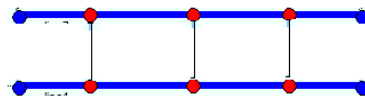
#### 4 plate fields



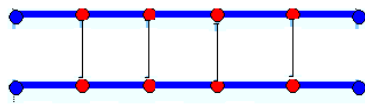
#### 6 plate fields



#### 8 plate fields



#### 10 plate fields



You can, similar to single optimization, select the checks that shall be runned. Also you can set the girder (frame) properties. This is used for calculating the weights.

With reference to the example above, max span mult is the multiplier for the 4 plate fields set up and min span mult is the weight multiplication for the 10 plate field set up. This is adopted because one can assume the required dimensions for the girder will reduce when more girders are added.

Minimum span and maximum span is the minimum and maximum span of the plate fields in meters.

Check for minimum section modulus	<input checked="" type="checkbox"/>	<b>Frame (girder data) for weight calculation:</b>	
Check for minimum plate thk.	<input checked="" type="checkbox"/>	Girder thickness	<input type="text" value="0.018"/>
Check for minimum shear area	<input checked="" type="checkbox"/>	Stiffener height	<input type="text" value="0.25"/>
Check for buckling (RP-C201)	<input checked="" type="checkbox"/>	Stiffener thickness	<input type="text" value="0.015"/>
Check for fatigue (RP-C203)	<input checked="" type="checkbox"/>	Stf. flange width	<input type="text" value="0"/>
Check for bow slamming	<input checked="" type="checkbox"/>	Stf. flange thickenss	<input type="text" value="0"/>
Check for local stf. buckling	<input checked="" type="checkbox"/>	For weight calculation of girder: Max span mult / Min span mult	
		<input type="text" value="1.2"/>	<input type="text" value="0.8"/>
		Maximum span / Minimum span ->	<input type="text" value="6"/> <input type="text" value="2"/>

Results are presented as seen next.

RUN OPTIMIZATION!

anysmart

algorithm information

Results seen next. Weight index is tot\_weight / max\_weight  
max\_weight is the highest total weight of the checked variations.  
Weight index of 1 is the heaviest calculated variation.

Plate fields	Fields length	Weight index	All OK?
*****			
4	6.0	1.0	True
6	4.0	0.768	True
8	3.0	0.765	True
10	2.4	0.825	True

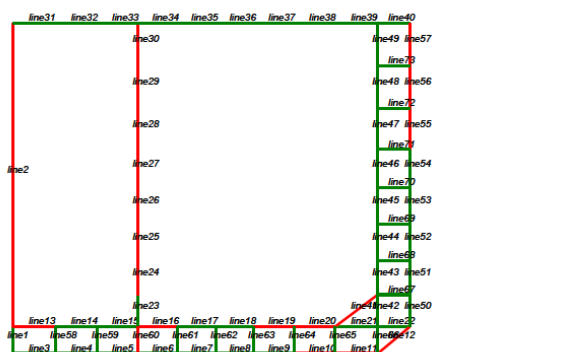
In this case 8 plate fields with length of 3 meter will give the lowest weight. 6 plate fields is almost equal.



ANYstructure report generator

User: [REDACTED]

Time : Mon, 06 Jan 2020 09:13:50 +0000



Compartments:

Compartments returned from search operation displayed below



Source: author's estimate, based on data from the Department of Statistics, (2002) (2003).

```
Name: comp2, content:
Min. elevation: 2.5, Max. elevation: 30.9
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_hai): (9.81, 3.0, 3.0)

Name: comp3, content:
Min. elevation: 2.5, Max. elevation: 30.900000000000002
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_hai): (9.81, 3.0, 3.0)

Name: comp4, content:
Min. elevation: 0.0, Max. elevation: 30.900000000000002
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_hai): (9.81, 3.0, 3.0)

Name: comp5, content:
Min. elevation: 0.0, Max. elevation: 2.5
Applied overpressure: 25000.0
(a_stat, a_dyn_loa, a_dyn_hai): (9.81, 3.0, 3.0)
```

```

***** line1 *****
Plate thickness: 14.0 [mm]      Stiffener spacing: 700.0 [mm]      Span: 2.5 [m]
Stiffener: 250.0x18.0 + 0.0x0.0
Fixation parameters: kps = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 40.0 [sigma_y1 = 100.0 sigma_y2 = 40.0 tau_xy = 5.0
ULS max pressure for line: 610.0 [kPa] Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/pant = 0/0/0 p_ext: loaded/ballast/pant = 0/40000.0/0
Section modulus: 360000 [mm^3] Min. section modulus: 80351 [mm^3] -> OK
Min plate thickness: 4.88 [mm] -> OK
Shear area: 4751 [mm^2] Min shear area: 296 [mm^2] -> OK
Highest buckling utilization: 0.41 -> OK
No fatigue results
Utilization percentage (highest calculated): 41%

***** line10 *****
Plate thickness: 18.0 [mm]      Stiffener spacing: 750.0 [mm]      Span: 3.8 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation parameters: kps = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 550.0 [kPa] Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/pant = 0/0/0 p_ext: loaded/ballast/pant = 0/40000.0/0
Section modulus: 1470000 [mm^3] Min. section modulus: 2073943 [mm^3] -> NOT OK
Min plate thickness: 15.76 [mm] -> OK
Shear area: 4656 [mm^2] Min shear area: 4129 [mm^2] -> OK
Highest buckling utilization: 1.39 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 141%

***** line11 *****
Plate thickness: 18.0 [mm]      Stiffener spacing: 750.0 [mm]      Span: 4.0 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation parameters: kps = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 550.0 [kPa] Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/pant = 0/0/0 p_ext: loaded/ballast/pant = 0/40000.0/0
Section modulus: 1470000 [mm^3] Min. section modulus: 2465181 [mm^3] -> NOT OK
Min plate thickness: 16.32 [mm] -> OK
Shear area: 4656 [mm^2] Min shear area: 4663 [mm^2] -> NOT OK
Highest buckling utilization: 1.63 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 167%

***** line12 *****
Plate thickness: 18.0 [mm]      Stiffener spacing: 750.0 [mm]      Span: 3.9051 [m]
Stiffener: 350.0x12.0 + 150.0x20.0
Fixation parameters: kps = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 100.0 sigma_y1 = 100.0 sigma_y2 = 100.0 tau_xy = 5.0
ULS max pressure for line: 590.0 [kPa] Pressure applied at: plate side
Fatigue pressure [Pa]: p_int: loaded/ballast/pant = 0/0/0 p_ext: loaded/ballast/pant = 0/40000.0/0
Section modulus: 1470000 [mm^3] Min. section modulus: 2516366 [mm^3] -> NOT OK
Min plate thickness: 16.89 [mm] -> OK
Shear area: 4656 [mm^2] Min shear area: 4875 [mm^2] -> NOT OK
Highest buckling utilization: 1.64 -> NOT OK
Fatigue (plate/stiffeners) utilization: 0.06 * DFF(2.0) = 0.12 (SN-curve = Ec)
Utilization percentage (highest calculated): 171%

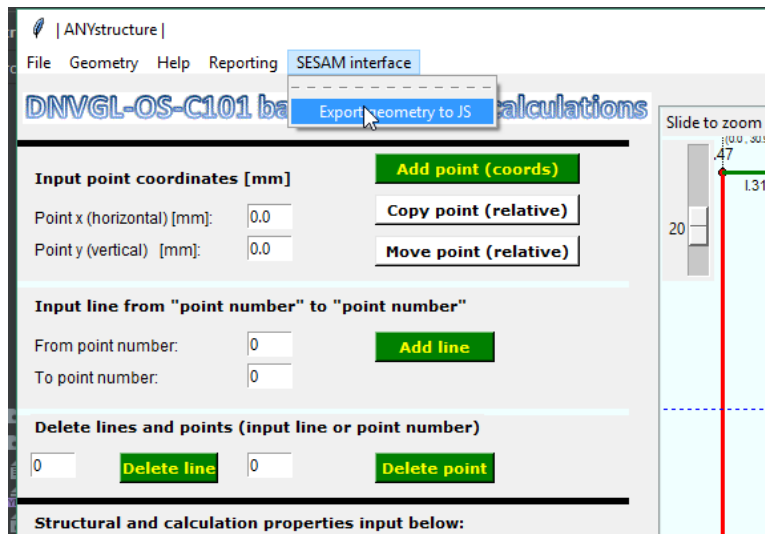
***** line13 *****
Plate thickness: 18.0 [mm]      Stiffener spacing: 775.0 [mm]      Span: 4.0 [m]
Stiffener: 375.0x12.0 + 150.0x18.0
Fixation parameters: kps = 1.0 kpp = 1.0, Bending moment factors km1/km2/km3 (support/field/support) = 12/24/12
Defined stresses [MPa]: sigma_x = 90.0 sigma_y1 = 90.0 sigma_y2 = 90.0 tau_xy = 5.0
ULS max pressure for line: 310.0 [kPa] Pressure applied at: plate side
Fatigue pressure: No pressures defined
Section modulus: 1500000 [mm^3] Min. section modulus: 1394615 [mm^3] -> OK
Min plate thickness: 12.48 [mm] -> OK
Shear area: 4932 [mm^2] Min shear area: 2725 [mm^2] -> OK
Highest buckling utilization: 1.06 -> NOT OK
No fatigue results
Utilization percentage (highest calculated): 106%

```



## Export to JS

ANYstructure can export points, lines and section properties to SESAM GeniE. A dialog will request a location to save the JS file. After that you can read the js file into GeniE.



The result is illustrated below:

